

海上河流相稠油油藏选择性堵水研究

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摘要:为了提高海上河流相稠油油藏堵水措施的有效性,结合渤中油田典型储层和流体特点,利用室内实验开展了海上河流相稠油油藏选择性堵水研究。对三种配制堵剂的注入能力、堵水有效期、封堵能力和对低渗层伤害程度等进行了分析评价,结果表明:堵剂A具有最好的注入性能,对低渗透层伤害程度最低;堵剂B具有最佳的封堵性能;堵剂C具有最长的堵水有效期。结合目标油田储层特征及海上平台操作要求,优选堵剂A在渤中25-1南油田E25井进行了现场试验。该井堵水后最大日增油约 35 m^3 ,含水率下降约10%,有效期396 d,累计增油达 $1.4 \times 10^4\text{ m}^3$,取得了较好的降水增油效果。

关键词:海上;稠油;选择性堵水;注入能力;有效期;封堵;储层伤害

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Research on Selective Water Plugging in Offshore Fluvial Heavy Oil Reservoir

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Abstract: In order to improve the effectiveness of water plugging in offshore fluvial heavy oil reservoirs, the selective water plugging study of offshore fluvial heavy oil reservoirs was carried out in combination with the typical reservoir and fluid characteristics of Bozhong Oilfield. Laboratory experiments were conducted to compare the performances of three kinds of plugging agents selected and prepared from four aspects: injection capacity, water plugging validity period, plugging capacity and damage degree to low permeability formation. The results show that plugging agent A has the best injection performance and the lowest permeability damage, plugging agent B has the best plugging performance, and plugging agent C has the longest water plugging validity. Combining reservoir characteristics of target oilfield and operation requirements of offshore platform, plugging agent A is selected as the best water plugging system and has been applied in Bozhong Oilfield. After water shutoff, the maximum daily oil increase of is about 35 m^3 , the water cut is reduced by about 10%, the validity period is 396 d, and the cumulative oil increase is $1.4 \times 10^4\text{ m}^3$, which has achieved a good effect.

Keywords: Offshore; Heavy oil; Selective water plugging; Injection capacity; Validity period; Block off; Reservoir damage

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0 前言

渤海油田稠油油藏储量大,埋藏深,在注水开发过程中,由于储层非均质性强、油水流量比大,加之开采速度快,使油井过早水淹^[1-3]。油井过早高含水会造成注采设备耗用,FPSO(浮式生产储油轮)处理产出液困难,加剧海管的腐蚀和结垢,使原油开采成本大幅上升。因此,必须采取高含水油井选择性堵水措施^[4-11]。

1 油田概况

渤中 25-1 南油田位于渤海湾盆地,是一个复杂的断裂背斜油藏。油田平均孔隙度为 30%,平均渗透率为 $1\ 000 \times 10^{-3} \mu\text{m}^2$,地下原油黏度 $50 \sim 274 \text{ mPa} \cdot \text{s}$,是高孔、高渗的稠油油藏。油田沉积类型为河流相沉积,平面非均质性强,注入水极易沿河道中心突进。目前油田综合含水 84%,已进入高含水阶段,优势渗流通道普遍发育,无效水循环加剧。亟待开展堵水研究,开发出与该油田地质特点相适应,与海上平台操作要求相匹配的堵水体系,以改善油田开发效果^[12-22]。

2 室内实验

2.1 实验材料及仪器

主要实验材料包括地层水样、油样、油酸、十二烷基苯磺酸、二甲苯、成磺酸钙、碳酸钙(800 目)、沥青粉、磺化沥青粉等。主要仪器包括超级恒温水浴槽、旋转黏度计、电动搅拌器、数显搅拌器、显微镜、摄像头、天平、物理模拟装置。

2.2 堵剂配制

利用目标油田油水样品,配制了 3 种堵剂:堵剂 A 1% MZ-18 + 3% BHN-12 + 混合油,堵剂 B 2% MZ-18 + 1% BHN-12 + 聚丙烯酰胺,堵剂 C 0.5% SH-1 + 2% CA-18。针对以上三种堵剂开展室内实验,对注入能力、堵水有效期、封堵效果和对低渗层伤害程度进行对比,以筛选满足实际油藏条件的最优堵水体系。

2.3 驱替实验步骤

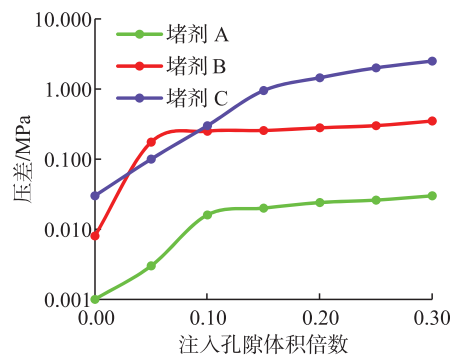
- 1) 筛选一定目数的砂子,将其洗净烘干后备用。
- 2) 用烘干后的砂子填于填砂管中,在常温下用地层水正向饱和,测定水相渗透率。
- 3) 称量饱和水之后填砂管的质量,结合填砂管的空管质量和填入砂子的质量,计算填砂管的孔隙体积 PV。
- 4) 将烘箱温度升至 $70 \text{ }^\circ\text{C}$ (油藏温度)并恒温。
- 5) 以不同的速率向填砂管中反向注入 0.3 PV 的地层水。
- 6) 向填砂管中正向注入地层水,注水速率为

0.5 mL/min,测量填砂管两端的压差,考察堵剂的堵水性能和耐冲刷性能。

3 性能对比评价

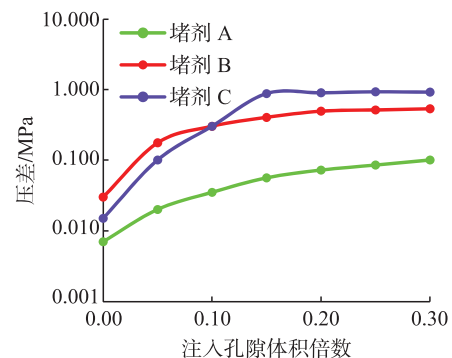
3.1 注入能力评价

分别做出三种堵剂在 $1\ 000 \times 10^{-3} \mu\text{m}^2$ 左右填砂管中注入和顶替压力曲线对注入压力和顶替压力进行对比,见图 1。由图 1 可知,在注入过程和顶替过程中,压力曲线特征不同。其中堵剂 C 压力最高,堵剂 B 次之,堵剂 A 最低,即堵剂 A 具有最佳的注入性能。



a) 注入压力曲线

a) Injection pressure curve



b) 顶替压力曲线

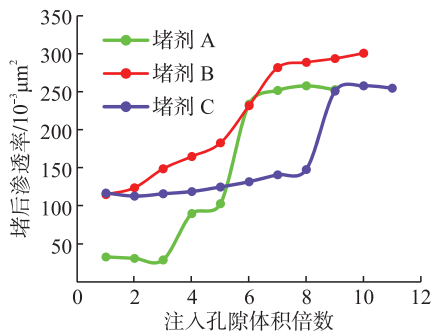
b) Replacement pressure curve

图 1 三种堵剂的压力曲线图

Fig. 1 Pressure curves of three plugging agents

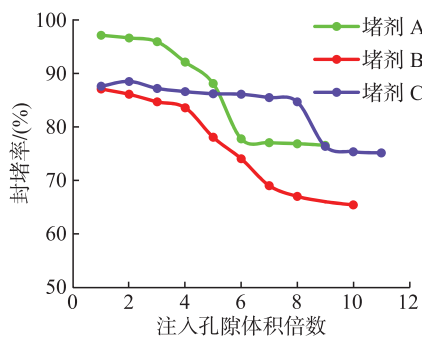
3.2 堵水有效期评价

分别做出三种堵剂在 $1\ 000 \times 10^{-3} \mu\text{m}^2$ 的填砂管中堵后渗透率和封堵率随注入孔隙体积变化的关系曲线以对比堵水有效期,见图 2。三种堵剂的堵水有效期不相同,但相差不大。其中堵剂 C 的封堵有效期最长,当注入 8 倍孔隙体积倍数时,封堵率保持在 86% 以上;堵剂 A 和堵剂 B 在注入 4 倍孔隙体积倍数时,封堵率开始下降,当注入 8 倍孔隙体积倍数时,封堵率分别下降到 76% 和 70% 左右。堵水有效期的评价为堵剂用量优化提供了依据。



a) 堵后渗透率

a) Sand permeability after plugging



b) 封堵率

b) Blocking rate

图2 堵水有效期的比较图

Fig. 2 Comparison of water plugging validity

3.3 封堵调剖效果评价

首先设置不同渗透率级差的双管模型,然后评价不同堵剂在不同级差下高低渗管的分流率之比,据此比较不同堵剂对非均质油层的改善程度,见图3。由图3可知,在不同的级差下,三种堵剂对高低渗管的封堵情况均不同。对于非均质程度较低的双管模型,三种堵水剂均表现出较好的封堵调剖能力,使模型的非均质程度得到大幅度改善,能够大幅度改善高、低渗模型的产液比例;对于非均质较严重的双管模型,封堵调剖能力相对较差。在相同的级差条件下,堵剂B的封堵调剖能力最好,平衡后高低渗管的分流率最为接近,使模型更趋于均质;堵剂A的封堵调剖能力要比堵剂C强一些,但在非均质程度较严重的条件下表现出与堵剂C相近的调整能力。

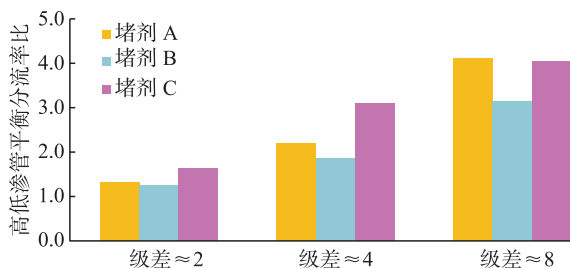


图3 不同堵剂的平衡分流率之比图

Fig. 3 The ratio of the equilibrium shunt rate of different plugging agents

3.4 储层伤害程度评价

根据实验结果评价不同渗透率级差下不同堵剂对低渗管的封堵率,据此比较三种堵剂对低渗储层的伤害程度,分析堵剂的选择性和智能性,结果见图4。由图4可知,在不同的渗透率级差下,三种体系对低渗管都表现出比较低的伤害,封堵率均在35%以下,并且随着级差的增大,低渗管的封堵率逐渐降低。表明堵剂主要进入的是高渗层,对低渗层的伤害较小,并且非均质程度越大,堵剂越容易进入高渗层,表现出较好的选择性封堵能力。在级差较小时,堵剂C对地层伤害最小;在级差较大时,堵剂A和堵剂C对低渗管的伤害要大于堵剂B。要根据油田储层的非均质程度选择适宜的堵剂。

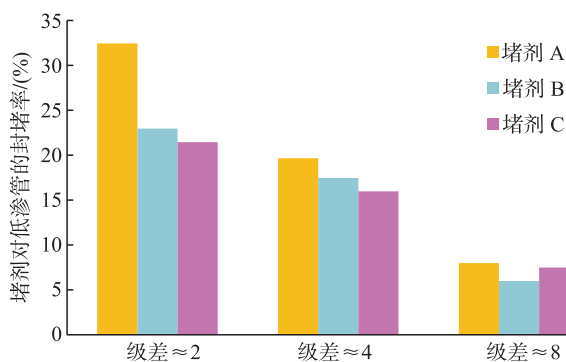


图4 不同堵剂对低渗管封堵率图

Fig. 4 Plugging rate of different plugging agents on low permeability pipes

4 矿场应用

海上油田具有安全注入压力窗口较小,流程处理要求高等特点。渤中25-1南油田属于海上河流相油田,储层平面非均质性强,渗透率级差大(平面渗透率级差3~5),综合考虑需选择易注入,易处理,储层伤害程度低的堵剂,因此选择堵剂A。该油田E25井主要开采层位为NmIV 8.2小层和NmV 3+5.1小层,施工前该井日产液150 m³,日产油15 m³,含水90%,测试显示主要出液和出水层位为NmV 3+5.1小层。2016年1月对该井堵水作业,堵水后产液量和含水持续下降,测试显示堵水后NmV 3+5.1小层产液比例由82%下降到70%,该井产液不均得到大幅改善,最大日增油达到了35 m³,含水下降约10%,有效期396 d,累计增油达1.4 × 10⁴ m³,取得明显效果。

5 结论

1) 利用室内实验对筛选配制的三种堵剂的注入性能、堵水有效期、封堵能力和对低渗层伤害程度进行分析评价,结果表明:堵剂A具有最佳的注入性能,在相同

渗透率条件下堵剂的注入压力和顶替压力是最低的;堵剂 B 具有最佳的封堵调剖性能;堵剂 C 具有最长堵水有效期和最低的低渗透层伤害性。三种体系各有所长,在实际应用中具有较大的选择空间。

2) 结合海上油田安全注入压力窗口小、环保排放要求高和平台空间小的具体条件,选择堵剂 A 在渤中 25-1 南油田 E 25 井进行堵水试验,结果表明该堵剂堵水效果好、增油明显。

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